

West Coast District Health Board

Te Poari Hauora a Rohe o Tai Poutini

Corporate Office High Street, Greymouth 7840 Telephone 03 769-7400 Fax 03 769-7791

11 December 2019



Official Information Request WCDHB 9373

I refer to your email dated 11 November 2019 requesting the following information under the Official Information Act from West Coast DHB regarding Manaakitanga mental health inpatient unit.

I understand the Manaakitanga mental health inpatient unit building's warrant of fitness issued by the Grey District Council is due to expire next year. Please provide the following information:

- 1. Any engineering reports for the unit produced in the last five years.
- 2. Any reports/documents on whether the unit meets earthquake code/reports on bringing it up to code.
- 3. The building's warrant of fitness or other certification issued by Grey District Council in 2019 and 2018.
- 4. Any applications for 2020.

Warrants of Fitness are issued annually by the responsible Territorial Authority. It confirms that specified systems in the compliance schedule (e.g. sprinklers) within a building have been inspected and maintained.

The information you have requested generally will not impact issue of a Building Warrant of Fitness (BWOF). Notwithstanding, please refer to the following appendices.

Appendix 1 -	Grey Hospital EQ rapid Assessments 23/11/2016
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Appendix 2 - Detailed Engineering Evaluation Grey Base Hospital 28/9/2012

Appendix 3 - Building Warrant of Fitness Grey Base Hospital (expires 1 July 2020)

Please note, we have redacted information pursuant to section 9(2)(a) of the Official Information Act to protect individual privacy.

I trust that this satisfies your interest in this matter.

You may, under section 28(3) of the Official Information Act, seek a review of our decision to withhold information by the Ombudsman. Information about how to make a complaint is available at <u>www.ombudsman.parliament.nz</u>; or Freephone 0800 802 602.

I trust that this satisfies your interest in this matter.

Please note that this response, or an edited version of this response, may be published on the West Coast DHB website after your receipt of this response.

Yours sincerely

Carolyn Gullery Executive Director Planning, Funding & Decision Support





23 November 2016

Opus International Consultants Ltd

JRMATION

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Greymouth Office

23 High Street

New Zealand

Craig Shaw Maintenance Manager West Coast District Health Board P O Box 387 Greymouth

Ref: 6-WWESE.10

Property inspected – Grey Hospital Buildings (various)

Dear Craig,

This report confirms the verbal advice provided to you on 23 November 2016 in relation to the rapid structural assessments Opus undertook of the Grey Hospital Buildings listed below (on Wednesday 23 November 2016) following the M7.8 earthquake which occurred on 14 November 2016:

- Boiler House Building,
- Acute and Community Mental Health Building,
- Laboratory Building,
- ED / Clinical Services Building,
- Morice Ward Building (Wards 1 and 2 North Building),
- Hannan Ward Building (Wards 3 and 4 Building),
- Kitchen Block Building,
- Child and Adolescent Mental Health Services (CAMHS).

The scope of our rapid structural assessments comprised of a brief visual inspection of the Buildings to ascertain the level of damage sustained to the primary structure and a brief external visual inspection of the neighbouring buildings and structures which we reasonably believe may impact the seismic performance of the Building.

Prior to carrying out these inspections we reviewed the original Opus Detailed Seismic Assessment Reports completed for these buildings (c2012-c2013) to confirm weaknesses identified in the assessments so that we could pay particular attention to these items in our inspection. We also reviewed previous photos of the Boiler House to assess whether there had been any increase in cracking at the junction between the Boiler House and Generator Buildings, and along the eastern wall of the Boiler House building.

The scope of our inspection is further detailed in the Earthquake Rapid Assessment Forms, which are attached to this letter.

Inspection Summary

In summary, our inspections noted the following observed damage:

• Negligible damage noted to buildings. Some cracking may have anecdotally worsened but generally no evidence of new damage to building.

Unless noted otherwise on the Earthquake Rapid Assessment Forms, we have not inspected any nonstructural hazards.

Based on our inspections, it is our assessment that the Building's seismic performance has not been significantly affected. The Buildings listed may therefore be occupied on the same basis as prior to the Earthquake. However, if you become aware of any changes in seismic performance of the neighbouring buildings or structures, please contact us immediately as the change may impact this assessment. In addition, aftershocks may cause more damage that may change this assessment and warrant further inspection of the building and/or neighbouring buildings or structures.

Although it is our assessment that the seismic performance of the buildings listed has not been significantly affected, if you are aware that a Building was Earthquake Prone or is subject to strengthening requirements, we recommend that you review the strengthening actions to ensure that they are still fit for purpose.

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We also recommend building maintenance staff carry out a full walk through of the entire hospital to identify any loose / damaged ceiling tiles so that these can be immediately repaired or replaced.

Do not hesitate to contact me if you require any further assistance.

Regards	
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Encl.: Earthquake	Rapid Assessment Forms
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Complex Residential and all Non-Residential Buildings Level 2

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If required add sketch on separate page showing extent and nature of the external risk factors.

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1 Collapse or partial collapse	0	0	01	0	0	11 Parapets, ornamentation, chimneys	0	0	Ø,	0	0
2 Building or storey leaning	0	,0	Ø	0	0	12 Cladding, glazing	0	0	Ø	0	0
3 Other:	Ø	0	0	0	0	13 Ceilings, light fixtures	V	0	0,	0	0
Structural Hazards*	N/A	А	в /	с	D	14 Interior walls, partitions	0	0	Ø,	0	Q
4 Foundations	0	0	0,	0	0	15 Access/egress (elevators, stairs, exits)	0	0	ø,	0	0
5 Roofs, floors	0	0	01	0	0	16 Significant fire saftey concerns	0	0	Ø	0	-0
6 Gravity systems (columns, beams, etc)	0	0	S'	0	0	17 Utilities (e.g. gas, electricity, waste water, plumbing)	0	0	0	0	0
7 Lateral systems (walls, frames, braces)	0	0	Ø,	0	0	18 Other:	0	0	,a	0	0
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EARTHQUAKE RAPID ASSESSMENT FORM – Complex Residential and all Non-Residential Buildings Level 2

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Complex Residential and all Non-Residential Buildings Level 2

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If required add sketch on separate page showing extent and nature of the external risk factors.

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Complex Residential and all Non-Residential Buildings Level 2

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If required add sketch on separate page showing extent and nature of the external risk factors.

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VERSION 01 - APRIL 2014

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Complex Residential and all Non-Residential Buildings Level 2

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Assessor Name*	9(2)(d)				
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Assessment Date	e* 23/16 Day Month Year	Assessment Time*	Hour Minute (to nearest half hour)		PM
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If required add sketch on separate page showing extent and nature of the external risk factors.

4 Other

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OHIBITED (At r	isk from	external factors)			E	Comple	te
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Complex Residential and all Non-Residential Buildings Level 2

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Assessor ID*		Authority*	WCOMB		
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Unit / Number*		C	1		1
Street*					
City/Town*	REYMOUT	TH			TTT
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Contact Name	RAZG SP	TAN	N ITTE		
-		aant Other	MAINTENANCE	MANA	100
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4 Other

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	-		Damag	e					Damag	е	
	N/A	Unknown	Minor or None	Moderate	Severe		N/A	Unknown	Minor or None	Moderate	Sever
Overall Hazard*	N/A	А	B /	С	D	Non-structural Hazards*	N/A	A	B	C	D
1 Collapse or partial collapse	0	0	0,	0	0	11 Parapets, ornamentation, chimneys	0	0	0,	0	0
2 Building or storey leaning	0	0	S	0	0	12 Cladding, glazing	0	0	0	0	0
3 Other:	0	Q	0	0	0	13 Ceilings, light fixtures	d	0	0	0	0
Structural Hazards*	N/A	A	в	C	D	14 Interior walls, partitions	0	0	0,	0	Q
4 Foundations	0	0	S,	0	0	15 Access/egress (elevators, stairs, exits)	0	0	Ø,	0	0
5 Roofs, floors	0	0	Ø	0	0	16 Significant fire saftey concerns	0	0	0	00	0
6 Gravity systems (columns, beams, etc)	0	0	Ø,	0	0	17 Utilities (e.g. gas, electricity, waste water, plumbing)	Ø,	0	0	0	0
7 Lateral systems (walls, frames, braces)	0	0	Ø,	0	0	18 Other:	0	0	Q	0	0
8 Diaphragms, horizontal bracing	0,	0	0	0	0	Commente: No 4	ev .d	ence	2 01	MOV	em
9 Precast connections	S,	0	0	0	0	D seismic s	epa	rate	xn G	etwe	er
10 Other:	0	0	0	0	0	Guildings	4	A.			
B2 Geotechnical Engin B3 Other:	neer arrange	d by buildin	g owner:	X		separate sneet	n require				
M M A R Y Observed Damage	Lev	el 2 Rap	id Asse	ssment	t Outco	me*	(12)	Circu	av Evta	nt*	
		CANIDE	USED (F	rom asses	sment no	known dangers)	9	Surve	By LXIE	Dortial	
Light or no damage	W	GAN DE				and a second second second		Exterio	or A	Partial	
Light or no damage	W V	RESTRIC	TED AC	CESS TO	PART(S)	OF THE BUILDING ONLY		Exterio	01	10.1	
Light or no damage	W V Y1C Y2C	RESTRIC	TED AC	CESS TO CESS – S	PART(S)	OF THE BUILDING ONLY RM ENTRY ONLY		Exteric	В (Comple	ete
Light or no damage Moderate damage	W (Y1C Y2C	RESTRIC	TED ACC	CESS TO CESS – S supervisi	PART(S) HORT TE on	OF THE BUILDING ONLY			B (Comple) Not acc	ete cessed
Light or no damage Moderate damage	W Y1C Y2C	RESTRIC RESTRIC with or Access to	CTED ACC CTED ACC without so be supe	CESS TO CESS – S supervisi	PART(S) HORT TE on A O Yes	OF THE BUILDING ONLY RM ENTRY ONLY B O No		Interior	в (с (г D (Comple Not acc	ete cessed
Light or no damage Moderate damage Heavy damage	W V Y1C Y2C R1C	RESTRIC RESTRIC With or M Access to ENTRY F	CTED ACC CTED ACC without so be supe PROHIBIT	CESS TO CESS - S supervisi rvised TED (At r	PART(S) HORT TE on A Yes isk from	OF THE BUILDING ONLY RM ENTRY ONLY B No external factors)		Interior	B (C (D (E (Comple Not acc Partial Comple	ete cessed ete
Light or no damage Moderate damage Heavy damage	W Y1 Y2 Y2 R1 R2 (2)(3)) RESTRIC With or Access to ENTRY F	CTED ACC CTED ACC without so be supe be supe PROHIBI	CESS TO CESS – S supervisi rrvised TED (At r TED (Sev	PART(S) HORT TE on A Yes isk from ere dama	OF THE BUILDING ONLY RM ENTRY ONLY B O No external factors) age to building)		Interior	B (C (D (E (Comple Not acc Partial Comple	ete cessed ete
Light or no damage Moderate damage Heavy damage	W Y1 Y2 R1 R2 (2)(a)	RESTRIC With or Access to ENTRY F	CTED ACC CTED ACC without : b be supe PROHIBI PROHIBI	CESS TO CESS – S supervisi rvised TED (At r TED (Sev	PART(S) HORT TE on A Yes isk from ere dama	OF THE BUILDING ONLY RM ENTRY ONLY B O No external factors) age to building)		Interior	B (C (T D (E (Comple Not acc Partial Comple	ete cessed ete
Light or no damage Moderate damage Heavy damage Assessor Signature [*] TES	W Y1 Y2 R1 R2 (2)(a)	RESTRIC RESTRIC with or Access to ENTRY F	CTED ACC CTED ACC without s be supe PROHIBI	CESS TO CESS – S supervisi rvised TED (At r TED (Sev	PART(S) HORT TE on A Yes isk from ere dama	OF THE BUILDING ONLY RM ENTRY ONLY B No external factors) age to building)		Interior	B (C (F E (Comple Not acc Partial Comple	ete cessed ete
Light or no damage Moderate damage Heavy damage Assessor Signature* TES Building		RESTRIC With or Access to ENTRY F	CTED ACC CTED ACC without : b be supe PROHIBIT PROHIBIT	CESS TO CESS - S supervisi rvised TED (At r TED (Sev	PART(S) HORT TE on A Yes isk from ere dama	OF THE BUILDING ONLY RM ENTRY ONLY B O No external factors) age to building)		Interior	B (C (C (E (Comple Not acc Partial Comple	ete cessed ete
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Light or no damage Moderate damage Heavy damage Assessor Signature* TES	W Y1 Y2 R1 R2 (2)(a)	RESTRIC RESTRIC RESTRIC RESTRIC Network Access to ENTRY F ENTRY F ENTRY F	CTED ACC CTED ACC without : b be supe PROHIBI PROHIBI	CESS TO CESS - S supervisi rvised TED (At r TED (Sev	PART(S) HORT TE on A Yes isk from ere dama	OF THE BUILDING ONLY RM ENTRY ONLY B No external factors) age to building)		Interior	B (C (F E (Comple Not acc Partial Comple	ete

VERSION 01 - APRIL 2014

EARTHQUAKE RAPID ASSESSMENT FORM – Complex Residential and all Non-Residential Buildings Level 2

1

Complex Residential and all Non-Residential Buildings Level 2

SESSMENT			Fields with asterisks (*) a	are mandatory, o	thers are opti
9(2) Assessor Name*	(a)				
Assessor ID*		Authority*	WCOHB		
Assessment Date*	231116 Day Month Year	Assessment Time*	Hour Minute (to nearest half hour)		PM
ILDING IDENT	IFICATION			,0'	
Building Name 🧜	IANNAN	NARD (NA	+2DS 3 84	1	
Unit / Number*	1				
Street*					
City/Town*	REYMOUT	TH			
GPS (Degree with 5 deci	imals after comma) SO	uth – ,	East		
Other ID or access		Photo ta		Photo ID.	
Contact Name	KATIG SI	THIN			
Type A	Owner BO Te	enant c 🕑 Other 🗹	VIAINTENANCE	MANY	HER
(Interview)					
Phone (with area code	None W Y	(1 R1 (2 R2 Date*	Day Month Year Tea	im ID*	
Phone (with area code Existing Placard* ()	a) None OW OY	(1 R1 (2 R2 Date*	Day Month Year Tea	im ID*	
Phone (with area code Existing Placard* ILDING DESCR Dimensions	a) None W Y Y RIPTION Constr. Age	(1 R1 (2 R2 Date*	Day Month Year Tea	Im ID*	g Type
Phone (with area code Existing Placard [*] (C ILDING DESCR Dimensions Storeys above ground	a) None W Y Y RIPTION Constr. Age	A Complex residential	Day Month Year Tea Structure Type	Cladding	g Type eer
Phone (with area code Existing Placard* () ILDING DESCR Dimensions Storeys above ground incl. ground floor	a) None W Y V RIPTION Constr. Age A <1935 B 1935-1976	A Complex residential B School	Day Month Year Tea Structure Type A Timber frame B Steel frame	Cladding	g Type eer panels
Phone (with area code Existing Placard* LDING DESCR Dimensions Storeys above ground incl. ground floor	a) None W Y Y XIPTION Constr. Age A <1935 B 1935-1976 C 1977-1984	A Complex residential B School C Commercial/Office	Day Month Year Tea Structure Type A Timber frame B Steel frame C Concrete frame	Cladding A Brick ven B Concrete C Steel	g Type eer panels
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Phone (with area code Existing Placard* ILDING DESCR Dimensions Storeys above ground incl. ground floor 2 Storeys below ground 0 1	a) None W Y Y V Y V Y V Y V Y V Y V Y V V V V V V V V V V V V V	A Complex residential B School C Commercial/Office D Industrial E Critical facility	Day Month Year Tea Day Month Year Tea Structure Type A Timber frame B Steel frame C Concrete frame D Concrete shear wall E Tilt-up concrete E Reinformed meconer	Cladding A Brick ven B Concrete C Steel D Glass E Lightweig	g Type eer panels
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Phone (with area code Existing Placard* ILDING DESCR Dimensions Storeys above ground incl. ground floor 2 Storeys below ground 0 1 Footprint (m ²) 1 2 Cotential Cause* Objects falling from adji	a) None W Y Constr. Age A <1935 B 1935-1976 C 1977-1984 D 1985-2000 E >2000 F Unknown	R1 Date* Building Type A Complex residential B School C Commercial/Office D Industrial E Critical facility F Public assembly G Other: Mospitul, non- essential ding ID or address:	Day Month Year Teat Day Month Year Teat Structure Type A Timber frame Timber frame B Steel frame C Concrete frame C Concrete shear wall E Tilt-up concrete F Reinforced masonry G Unreinforced masonry H Other: Other: Concrete	Im ID*	g Type eer panels ght B No

4 Other

0

0

			Damay	0					Damage			
	N/A	Unknown	Minor or None	Moderate	Severe		N/A	Unknown	Minor or None	Moderate	Seve	
Overall Hazard*	N/A	A	в	С	D	Non-structural Hazards*	N/A	A	В	С	D	
1 Collapse or partial collapse	0	0	ø,	0	0	11 Parapets, ornamentation, chimneys	V	0	0	0	0	
2 Building or storey leaning	0,	0	Ø	0	0	12 Cladding, glazing	0	0	0	0	0	
3 Other:	0	0	0	0	0	13 Ceilings, light fixtures	0	0	Ø	0	0	
Structural Hazards*	N/A	A	в	с	D	14 Interior walls, partitions	0	0	Ø,	0	Ø	
4 Foundations	0	0	Ø,	0	0	15 Access/egress (elevators, stairs, exits)	0	0	ø,	0	0	
5 Roofs, floors	0	0	S	0	0	16 Significant fire saftey concerns	0	0	0	0	0	
6 Gravity systems (columns, beams, etc)	0	0	Ø,	0	0	17 Utilities (e.g. gas, electricity, waste water, plumbing)	d	0	0	0	0	
7 Lateral systems (walls, frames, braces)	0	0	Ø	0	0	18 Other:	Ø	0	,a	0	0	
8 Diaphragms, horizontal bracing	0	0	0	0	0	Comments			\leftarrow			
9 Precast connections	ø	0	0	0	0			N				
10 Other:	Ø	0	0	0	0		0	d.				
B CLevel 2 Rapid Assessm (tick below if particular ex	None Level 2 Rapid Assessment (tick below if particular expertise is required)					an required B Barricades already in place B Immed ant (add diagram on C Barricades required B action					ured	
Recommended furth	er Ass	essmen	t*	Safety	Cordon	* Barricades	*		Urge	ency of		
A None			-	A CNO	ne required	d A ONone rev	quired		A Standard B Immediate			
B O Level 2 Rapid Assessm	nent			B Oco	rdon requi	red B O Barricad	les alread	ly in place				
(lick below it particular ex		Describe	extent (add	diagram on C Barricad	les requir	bo		action requ	iired			
B1 OStructural Enginee	r			separate :	sheet if req	uired) Describe exten	t (add dia	agram on				
B1 Structural Enginee	neer			separates	sheet if req	uired) Describe exten separate sheet	t (add dia if require	agram on ad)	-			
B1 Structural Enginee B2 Geotechnical Enginee B3 Other:	neer	d by buildin		separate :	sheet if req	uired) Describe exten separate sheet	t (add dia if require	agram on ad)]			
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C Further evaluation to be	r neer e arrange	d by buildin	g owner:	separate s	sheet if req	uired) Describe exten separate sheet	t (add dia if require	agram on ad)				
B1 Structural Enginee B2 Geotechnical Enginee B3 Other: C Further evaluation to be	r neer e arrange	d by buildin	g owner:	separate s	sheet if req	uired) Describe exten separate sheet	t (add dia if require	agram on ad)				
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C Further evaluation to be	ir neer e arrange	d by buildin	g owner:	separate s	sheet if req	Uired) Describe exten separate sheet	t (add dia if require	agram on ad)				
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C Further evaluation to be	ir neer e arrange	d by buildin	g owner:	separate :	sheet if req	uired) Describe exten separate sheet	t (add dia if require	agram on ad)				
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C Further evaluation to be MMARY Observed Damage	n neer e arrange	d by buildin	g owner:	essment	t Outco	uired) Describe exten separate sheet	(add dia if require	sgram on ad)	ey Exte	nt*/		
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C Further evaluation to be MMARY Observed Damage Light or no damage	e arrange	d by buildin	g owner: id Asse USED (F	essment rom asset	t Outco	Describe exten separate sheet	(add dia if require	Igram on id) Surve	ey Exte	nt* Partial		
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C C Further evaluation to be MMARY Observed Damage Light or no damage	arrange	d by buildin	g owner: id Asse USED (F	essment rom asset	t Outco ssment no	Describe exten separate sheet	(add dia if require	Surve Exteric	ey Exte or B (nt* Partial Comple	ete	
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C C Further evaluation to be MMARY Observed Damage Light or no damage Moderate damage	r neer e arrange Leve W Y1 Y2	d by buildin el 2 Rap CAN BE RESTRIC With or	g owner, id Asse USED (F CTED AC CTED AC	essment rom asset CESS TO CESS - S supervisi	t Outco ssment no PART(S) HORT TE	me* b known dangers) OF THE BUILDING ONLY RM ENTRY ONLY	(add dia if require	Surve Exteric	ey External A (B (C (Partial Comple	ete	
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C Further evaluation to be MMARY Observed Damage Light or no damage Moderate damage	r neer e arrange V1 Y1 Y2	d by buildin el 2 Rap CAN BE RESTRIC With or Access to	g owner. id Asse USED (F CTED AC CTED AC CTED AC	essment rom asset CESS TO CESS – S supervisi ervised	t Outco ssment no PART(S) HORT TE ion A Yes	me* pknown dangers) OF THE BUILDING ONLY RM ENTRY ONLY B No	(add dia if require	Surve Exteric	ey Exter or B (r D 0	Partial Comple Not acc	ete	
B1 Structural Enginee B2 Geotechnical Engine B3 Other: C Further evaluation to be MMARY Observed Damage Light or no damage Moderate damage	r neer e arrange Lev W Y1 Y2 R1	d by buildin el 2 Rap CAN BE RESTRIC RESTRIC With or Access to ENTRY I	g owner; id Asse USED (F CTED AC CTED AC CTED AC Without o be supe PROHIBI	essment rom asset CESS TO CESS - S supervise trvised	t Outco ssment no PART(S) HORT TE ion A Yes isk from	me* bknown dangers) OF THE BUILDING ONLY RM ENTRY ONLY B No external factors)	(add dia if require	Surve Exterio	ey Exte or F C (F E (Partial Comple Not acc Partial Comple	ete	

EARTHQUAKE RAPID ASSESSMENT FORM - Complex Residential and all Non-Residential Buildings Level 2

Complex Residential and all Non-Residential Buildings Level 2

AS	SESSMENT			Fields with asterisks (*)	are mandatory, others are optional.
1	Assessor Name*	(2)(a)	Authority*	NCDHB	
2	Assessment Date	* 231116 Day Month Year	Assessment Time*	Hour Minute (to nearest half hour)	AM BOPM
BU	ILDING IDEN	TIFICATION			10
3	Building Name Unit / Number* Street*	KITCHEN I I	BLOCK		
	City/Town*	GREYMOUT	U		
	GPS (Degree with 5 de	ecimals after comma) Sout	h – ,	East	
	Other ID or access		Photo ta	ken AONO BOYes	Photo ID.
4	Contact Name Type	A Owner B Ten	ant c Other	MAINTENANCE	E MANACIER
	Phone (with area code				
5	Existing Placard*		R1 R2 Date*	Day Month Year Tea	am ID*
BU	ILDING DESC	RIPTION		and the second second	
6	Dimensions	Constr. Age	Building Type	Structure Type	Cladding Type
	Storeys above ground incl. ground floor	A <1935 B 1935-1976	A Complex residential B School	A Timber frame	A Brick veneer B Concrete panels

Incl. ground floor	B 1935-1976	B O School	B O Steel frame	B Concrete panels
	C O 1977-1984	C Commercial/Office	C O Concrete frame	C Steel
Storeys below ground	D () 1985-2000	D O Industrial	D Concrete shear wall	D Glass
OI PLOOM	E >2000	E Ocritical facility	E O Tilt-up concrete	E Lightweight
Footprint (m ²)	FOUnknown	F Public assembly	F Reinforced masonry	F Other:
X50		G Other:	G Unreinforced masonry	
		Kitchen	H Other:	
R				
			1	

EXTERNAL RISKS 7 Potential Cause*

[}=]

Potential Cause*	AYes	в No
Objects falling from adjacent buildings. Adjacent building ID or address:	0	ø
2 Land instability above	0	C
3 Land instability below	0	Ø
4 Other	0	V

If required add sketch on separate page showing extent and nature of the external risk factors.

		_	Damag	le					Damag	e	
	N/A	Unknown	Minor or None	Moderate	Severe		N/A	Unknown	Minor or None	Moderate	Sever
Overall Hazard*	N/A	A	В	с	D	Non-structural Hazards*	N/A	А	В	С	D
1 Collapse or partial collapse	0	0	V	0	0	11 Parapets, ornamentation, chimneys	V	0	0	0	0
2 Building or storey leaning	0	0	Ø	0	0	12 Cladding, glazing	0	0	V	0	0
3 Other:	Ø	0	0	0	0	13 Ceilings, light fixtures	0	0	Ø	0	0
Structural Hazards*	N/A	A	в	С	D	14 Interior walls, partitions	0	0	Ø,	0	0
4 Foundations	0	0	Ø,	0	0	15 Access/egress (elevators, stairs, exits)	0	0	Ø,	0	0
5 Roofs, floors	0	0	0	0	0	16 Significant fire saftey concerns	0,	0	Q	0	0
6 Gravity systems (columns, beams, etc)	vity systems of the system of the syst					17 Utilities (e.g. gas, electricity, waste water, plumbing)	Ø,	0	0	0	0
7 Lateral systems (walls, frames, braces)	0	0	S,	0	0	18 Other:	Q	0	0	0	0
8 Diaphragms, horizontal bracing	0	0	Ø	0	0	Comments: Some	ple	exist	nac	rall	ing
9 Precast connections	Ø	0	0	0	0	avound doo	51	600	tele	w. S	na
10 Other:	V	0	0	0	0	crack opp	arte	2 RA	fema	110	on
101			_			G			sugg	ested a	ction*
GGESTED FUR	HER	RACT	IONS					_			
Recommended furthe	er Asse	essment	*	Safety	Cordon	* Barricades'	+		Urge	ncy of	
A None		_	-	ATONO	ne require		wirod		sugg	Esteu de	cuon
B O Level 2 Rapid Assessm	ent			B O Co	rdon requir	B Barricade	es alread	y in place	вО	Immediate	
B1 Structural Engineer	ertise is	required)		Describe a	extent (add	Idiagram on C O Barricade	es requir	ed		action requ	ired
B2 Geotechnical Engin	eer					Describe extent separate sheet i	f require	gram on d)			
B3 Other:		_									
C Further evaluation to be	arrange	d by buildin	g owner:								
			X								_
MMARY		0	V						-	-	
MMART		SV.					-				
Observed Damage	Leve	el 2 Rapi	id Asse	essment	t Outco	me*	(12)	Surve	ey Exte	nt*	
Light or no damage	wC	CAN BE	USED (F	rom asses	ssment no	o known dangers)		-	A	Partial	
	Y1C	RESTRIC	TED AC	CESS TO	PART(S)	OF THE BUILDING ONLY		Exterio	в	Comple	ete
Moderate damage	Y2C	RESTRIC	TED AC	CESS – S	HORT TE	RM ENTRY ONLY			c (Not acc	essed
		Access to	be supe	ervised	A O Yes	B 🔿 No		Interior	DG	Partial	
1 V	R1	ENTRY	ROHIBI	TED (At r	isk from	external factors)		1.000	F	Comple	ate
Heavy damage	R2	ENTRY	ROHIBI	TED (Sev	ere dama	age to building)			-	Joompie	
· · · · · *	(Z)(d)								_		
Assessor Signature*											
TES											
						and the second second				-	
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											_

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Complex Residential and all Non-Residential Buildings Level 2

C. C. C. T. L. T.	9(2)(a)		The los with dote it should be	and manuatory, c	niters are
Assessor Name*					
Assessor ID*		Authority*	NCOHB		
Assessment Da	te* 231116 Day Month Year	Assessment Time	+ (225) Hour Minute (to nearest half hour)		РМ
ILDING IDE	NTIFICATION			.0'	
Building Name	CHILDR	ADOLESC	ENT MEN	TAL	HE
Unit / Number*	1071	5	ERVICES (CAMH	5)
Street*	COMPER	STREET	TITOL		
City/Town*	GREYMOU	TM			
GPS (Degree with 5	decimals after comma) So	uth,	East		
Other ID or acces	s	Photo ta	ken AONO BOYes	Photo ID.	
Contact Name	CRAIGSI	HAN			
Туре	A Owner B O Te	enant c Other	MAINTENANCE	E MAA	ACH
Existing Placard*		1 OR1 Date*	Tea	am ID*	
Existing Placard*	CRIPTION	(1 OR1 (2 OR2 Date*	Day Month Year Tea	am ID*	
Existing Placard [*] ILDING DES Dimensions	CRIPTION Constr. Age	Building Type	Day Month Year Tea	am ID*	g Type
Existing Placard [*] ILDING DES Dimensions Storeys above groun	None W CRIPTION Constr. Age d A < <1935	Building Type	Day Month Year Tea Structure Type	am ID*	g Type
Existing Placard [*] ILDING DES Dimensions Storeys above groun- incl. ground floor	None W CRIPTION Constr. Age d A A <1935	Building Type	Day Month Year Tea Structure Type A Timber frame B Steel frame	Claddin	g Type neer panels
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4 Other

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			Damag	e					Damag	е	
	N/A	Unknown	Minor or None	Moderate	Severe		N/A	Unknown	Minor or None	Moderate	Sever
Overall Hazard [*]	N/A	A	в	с	D	Non-structural Hazards*	N/A	A	В	С	D
1 Collapse or partial collapse	0	0	S	0	0	11 Parapets, ornamentation, chimneys	C	0	0	0	0
2 Building or storey leaning	0	0	S	0	0	12 Cladding, glazing	0	0	Ø	0	0
3 Other:	Ø	0	0	0	0	13 Ceilings, light fixtures	Ø	0	0	0	0
Structural Hazards [*]	N/A	А	В	С	D	14 Interior walls, partitions	Ø	0	0	0	Q
4 Foundations	0	0	S,	0	0	15 Access/egress (elevators, stairs, exits)	Ø	0	0	0	(9)
5 Roofs, floors	0	0	0	0	0	16 Significant fire saftey concerns	Ø	0	0	0	0
6 Gravity systems (columns, beams, etc)	0	0	S	0	0	17 Utilities (e.g. gas, electricity, waste water, plumbing)	Ø	0	0	0	0
7 Lateral systems (walls, frames, braces)	0	0	S	0	0	18 Other:	Q	0	0	0	0
8 Diaphragms, horizontal bracing	0	0	V	0	0	Comments		-	\leftarrow		
9 Precast connections	0	0	0	0	0	Commenta.		R			
10 Other:	C	0	0	0	0		0	4.			
(tick below if particular exp B1 O Structural Engineer B2 O Geotechnical Engin	ertise is	required)		Describe separates	extent (add sheet if req	diagram on uired) C O Barricad Describe exten separate sheet	les requir t (add dia if require	ed gram on d)		action requ	iired
B1 O Structural Engineer				separate s	sheet if req	uired) Describe exten	t (add dia	gram on			
B3 Other:	661				1			- (
C O Further evaluation to be	arrange	d by buildin	g owner:	X					ĺ		
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Observed Damage	Leve	el 2 Rap	id Asse	ssmen	t Outco	me*	(12)	Surve	ey Exte	nt*	
Light or no damage	w 💽	CAN BE	USED (F	rom asses	ssment no	known dangers)			A (Partial	
	Int or no damage W CAN BE USED (F				PART(S)	OF THE BUILDING ONLY		Exterio	B (Comple	ete
	Y1C	Y2 RESTRICTED ACC				SHORT TERM ENTRY ONLY			C (Not accessed		
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EARTHQUAKE RAPID ASSESSMENT FORM – Complex Residential and all Non-Residential Buildings Level 2



Detailed Engineering Evaluation Quantitative Assessment Report

Grey Base Hospital Acute & Community Mental Health Services Building



Detailed Engineering Evaluation

Quantitative Assessment Report

Grey Base Hospital Acute & Community Mental Health Services Building



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Date: Reference: Status:

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Executive Summary

The West Coast District Health Board appointed Opus International Consultants (Opus) to carry out a detailed seismic assessment of the Acute & Community Mental Health building at Grey Base Hospital in Greymouth. The key outcome required of this assessment was to ascertain the anticipated seismic performance of the structure and to compare this performance with current design standards. Opus was also asked to provide conceptual strengthening options to improve the building's seismic performance, with a target of meeting at least 67% of the New Building Standard (%NBS) for a building with Importance Level 2 (IL2).

Findings of the assessment are:

a) The building has a seismic capacity of 19%NBS along the building (North-South) and 15%NBS across the building (East-West). Therefore this building is classified as Earthquake Prone, as defined by the Building Act, and is a High Risk building when classified in accordance with NZSEE [2].

Strengthening is required under the Building Act (2004) and Greymouth District Council (GDC) policy on Earthquake Prone Buildings [6]. GDC policy requires this building to be strengthened to achieve a minimum seismic performance of 67% NBS within 12 years.

- b) Liquefaction and lateral spreading damage is not expected in an Ultimate Limit State (ULS) earthquake at the site. Any differential settlement would be due to large cyclic loads causing permanent settlements of the foundations. These differential settlements are hard to quantify, but generally are reasonably minor should not cause any issues from an ULS perspective.
- c) A broad design concept to bring the building up to 67%NBS has been considered.

Possible strengthening to improve seismic performance of the building could include the following:

- Develop a bracing plan, calculating the length, type and location of new bracing elements required on the first floor, and
- Remove existing first floor timber framed wall linings, install required hold-down restraints at the base of the wall and re-line walls with GIB bracing, or

Install steel straps with hold downs over the top of existing timber walls to act as bracing bays. Note that given the obtrusive nature of this strengthening option, it is unlikely to be a suitable long term solution.

Recommendations:

As this building is Earthquake Prone, GDC policy [6] requires strengthening work to improve the building performance to a minimum of 67%NBS to be completed within 12 years.



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We recommend that a staged strengthening approach as detailed below is followed in order to understand and manage the economic impact of any proposed remedial actions. Specifically we recommend that:

a) The implications of the IL2 classification for this building be carefully considered prior to carrying out any future works on this building, noting that with an IL2 classification, this building is not expected to remain operational post-disaster.

An IL2 classification may also limit future use of the building.

- b) An outline scheme for structural strengthening with a view to achieving at least 67%NBS should be further developed followed by costing by a quantity surveyor.
- c) A quantity surveyor is engaged to determine the costs for strengthening the building.
- d) Detailed design of a scheme for the strengthening of the structure is carried out.

In addition to the seismic strengthening scheme, there are several issues that were identified during the inspection that warrant further investigation:

- There is cracking and possibly spalling of concrete on the vent sills in the lower ground floor external walls on gridline K between gridline 1 and 8. This type of deterioration has also been identified elsewhere in the hospital and we recommend that chloride intrusion testing be carried out. This will help to identify whether there are any major issues with concrete deterioration of the building.
- There is extensive cracking in lower ground floor walls surrounding the storage area between gridline 1 and 8 and gridline K and M. These walls have been plastered and the reason why is unclear. This may indicate some underlying issue which we recommend be investigated further.
- The brick veneers at lower ground level are typically pulling away from the concrete walls behind. This may be due to the corrosion of galvanised tie wires behind the brick veneers. It is recommended that some brickwork be removed to allow for inspection of the tie-back and the investigation of other possible causes for the separation. The ground floor brick veneers were not inspected and we recommend that any further investigation / inspection include these also.





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1 Introduction

Opus International Consultants Limited (Opus) has been engaged by the West Coast District Health Board (WCDHB) to undertake a detailed seismic assessment of the Acute & Community Mental Health Services Building at Grey Base Hospital in Greymouth.

The purpose of the assessment is to determine the likely seismic performance of the building and also if the building is classed as being Earthquake Prone in accordance with the Building Act 2004.

The seismic assessment and reporting have been undertaken based on the qualitative and quantitative procedures detailed in the Detailed Engineering Evaluation Procedure (DEEP) document (draft) issued by the Structural Engineering Society (SESOC) on 19 July 2011.

It was advised by the WCDHB that the Acute & Community Mental Health Building is to be assessed as an Importance Level 2 (IL2) building.

Definitions of an IL2 building can be found in AS/NZS 1170.0:2002 (Structural design actions Standard) [10]. The definition of an IL2 building (extract from Table 3.2 [10]) is: "Normal structures and structures not in other importance levels".

This designation will require the earthquake return period factor for the ultimate limit state of $R_u = 1.0$ (over an assumed building design life of 50 years) to be used. For the same design life an IL3 building has an earthquake return period factor of $R_u = 1.3$. Practically this means that an IL3 building is expected to withstand an earthquake of approximately 30% stronger than that expected of an IL2 building.

2 Compliance

This section contains a brief summary of the requirements of the various statutes and authorities that control activities in relation to buildings in New Zealand at present.

2.1 Building Act

Several sections of the Building Act are relevant when considering structural requirements:

Section 112 - Alterations

This section requires that an existing building complies with the relevant sections of the Building Code to at least the extent that it did prior to the alteration.

This effectively means that a building cannot be weakened as a result of an alteration (including partial demolition).

Section 115 – Change of Use

This section requires that the territorial authority (in this case Grey District Council (GDC)) is satisfied that the building with a new use complies with the relevant sections of the Building Code 'as near as is reasonably practicable'.



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This is typically interpreted by GDC as being between 67% and 100% of the strength of an equivalent new building.

Section 122 – Earthquake Prone Buildings

This section defines a building as earthquake prone if its ultimate capacity would be exceeded in a 'moderate earthquake' and it would be likely to collapse causing injury or death, or damage to other property.

A moderate earthquake is defined by the building regulations as one that would generate loads 33% of those used to design an equivalent new building on the same site.

Section 124 – Powers of Territorial Authorities

This section gives the territorial authority the power to require strengthening work within specified timeframes or to close and prevent occupancy to any building defined as dangerous or earthquake prone.

Section 131 – Earthquake Prone Building Policy

This section requires the territorial authority to adopt a specific policy for earthquake prone, dangerous and insanitary buildings.

2.2 Grey District Council Policy

Grey District Council adopted their Earthquake Prone, Dangerous and Insanitary Building Policy in 2006. This policy was amended in 2011 and an updated policy was adopted on 14 February 2011 [6].

The 2011 amendment includes the following:

- An audit process for identifying pre-1976 potentially Earthquake Prone commercial buildings within the 2011 financial year.
- The introduction of maximum timeframes for undertaking further structural assessment of buildings identified through the GDC audit process as being potentially Earthquake Prone.

The introduction of maximum timeframes for strengthening Earthquake Prone buildings (1-25 years) dependent on the importance level and age of the building.

Building Code

The New Zealand Building Code outlines performance standards for buildings and the Building Act requires that all new buildings comply with this code. Compliance Documents published by the Department of Building and Housing can be used to demonstrate compliance with the Building Code.

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2.4 Institution of Professional Engineers New Zealand (IPENZ) Code of Ethics

One of the core ethical values of professional engineers in New Zealand is the protection of life and safeguarding of people. The IPENZ Code of Ethics requires that:

Members shall recognise the need to protect life and to safeguard people, and in their engineering activities shall act to address this need.

- 1. Giving Priority to the safety and well-being of the community and having regard to this principle in assessing obligations to clients, employers and colleagues.
- Ensuring that responsible steps are taken to minimise the risk of loss of life, injury or suffering which may result from your engineering activities, either directly or indirectly.

All recommendations on building occupancy and access must be made with these fundamental obligations in mind.

3 Earthquake Resistance Standards

For this assessment, the building's earthquake resistance is compared with the current New Zealand Building Code requirements for a new building constructed on the site. This is expressed as a percentage of new building standard (%NBS). The loadings are in accordance with the current earthquake loading standard NZS1170.5 [1].

A generally accepted classification of earthquake risk for existing buildings in terms of %NBS that has been proposed by the NZSEE 2006 [2] is presented in Figure 3.1 below.

Description	Grade	Risk	%NBS	Existing Building Structural Performance		Improvement of Structu	ral Performance
					┍╼	Legal Requirement	NZSEE Recommendation
Low Risk Building	A or B	Low	Above 67	Acceptable (improvement may be desirable)		The Building Act sets no required level of structural improvement	100%NBS desirable. Improvement should achieve at least 67%NBS
Moderate Risk Building	S	Moderate	34 to 66	Acceptable legally. Improvement recommended		This is for each TA to decide. Improvement is not limited to 34%NBS.	Not recommended. Acceptable only in exceptional circumstances
High Risk Building	D or E	High	33 or lower	Unacceptable (Improvement required under Act)		Unacceptable	Unacceptable

Figure 3.1: NZSEE Risk Classifications Extracted from table 2.2 of the NZSEE 2006 AISPBE Guidelines

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Table 3.1 below compares the percentage NBS to the relative risk of the building failing in a seismic event with a 10% risk of exceedance in 50 years (i.e. 0.2% in the next year)

Percentage of New Building Standard (%NBS)	Relative Risk (Approximate)	
>100	<1 time	
80-100	1-2 times	
67-80	2-5 times	
33-67	5-10 times	
20-33	10-25 times	/
<20	>25 times	>

Table 3.1: %NBS compared to relative risk of failure

3.1 Minimum and Recommended Standards

Based on governing policy and recent observations, Opus makes the following general recommendations:

3.1.1 Cordoning

 Where there is an overhead falling hazard or potential collapse hazard of the building, the areas of concern should be cordoned off to prevent access (for guidance with this issue refer to GDC guidelines on Dangerous Buildings [6]).

3.1.2 Strengthening

- Industry guidelines (NZSEE 2006 [2]) strongly recommend that every effort be made to achieve improvement to at least 67%NBS. A strengthening solution to anything less than 67%NBS would not provide an adequate reduction to the level of risk.
- GDC policy [6] requires Earthquake Prone buildings of Importance Level 2 (IL2) be strengthened to a minimum of 67% NBS. The GDC policy [6] requires an Earthquake Prone building, designed to the 1976 codes be strengthened within twelve years.

It should be noted that full compliance with the current building code requires building strength of 100%NBS.

3.1.3 Our Ethical Obligation

 In accordance with the IPENZ code of ethics, we have a duty of care to the public. This obligation requires us to identify and inform GDC of potentially dangerous buildings; this would include earthquake prone buildings.



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4 Background Information

4.1 Building Description

The Grey Base Hospital – Acute & Community Mental Health Services Building is a two storey Reinforced Concrete (RC) dual frame / wall building with internal timber framed first floor walls and roof structure. Structural drawings for the building are dated November 1977 and the building is believed to have been constructed circa 1978. Figure 4.1 below shows an aerial view of the building.



Figure 4.1: Aerial photo showing location of the Acute & Community Mental Health Services building at Grey Base Hospital.

The building contains both irregular geometries in plan and elevation. The north-western end of the building consists of two storeys plus a basement level and has an overall plan dimension of 25.9m long x 26.4m wide. The south-eastern end of the building consists of two storeys and has an overall plan dimension of 51.4m x 10.8m. The north western and south eastern ends are not seismically separated. They are linked together at the ground and first floor level by a 140mm thick concrete slab and will behave as one under seismic events.

For the purposes of this report and to keep with the naming convention used on site, the top level will be referred herein as the ground floor. Below ground floor is the lower ground floor and beneath this is the basement.

The ground floor structure consists of a pierced RC shear wall around the perimeter with internal timber framed walls supporting a timber framed roof structure. The roof structure consists of joists spanning between internal timber walls and external concrete walls. The



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roof consists of a particle board overlay supporting a membrane cladding system. The roof is non-trafficable and accessible for maintenance purposes only. Below the ground floor level, the concrete floor slab is supported on RC walls and frames.

The foundations consist of a continuous strip foundation underneath the RC walls and individual pad footings underneath individual columns. Pad footings are linked together with RC groundbeams.

All stairways are cast in situ reinforced concrete.

The building is also connected to the Physiotherapy/Laboratory Block with a linkage slab. There is a seismic gap of 25mm between the two structures.

There are a number of non-structural timber framed partitions within the building separating various parts of the building.

The exterior cladding consists of 110mm thick brick veneer, supported on nibs cast in the concrete walls. Precast concrete fins are positioned at the vertical edges of all first floor windows for aesthetics purposes. These are dowelled into the concrete walls.



Figure 4.2 below shows the building elevations.



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4.2 Building use

The Acute & Community Mental Health Building has offices, meeting rooms and an an acute mental health inpatient unit located on the ground floor. This inpatient unit provides overnight accomodation and is limited to a maximum of five beds.

The lower ground floor of the building contains offices and meeting rooms.

4.3 Gravity Load Resisting System

The main gravity load resisting system timber framed walls and perimeter RC walls. The main gravity load resisting system at lower ground floor and basement level consists of RC frames and walls.

The RC walls are supported on a continuous RC perimeter foundation extending around the building. The internal RC columns are supported on individual pad footings which are linked together by RC groundbeams.

4.4 Lateral Load Resisting System

Lateral loads are resisted in the transverse and longitudinal directions as indicated below.

4.4.1 Transverse Loading

Lateral loads in the transverse direction are resisted through the in-plane action of timber and RC walls. Timber framed bracing walls transfer the lateral loading from the roof level to the ground floor RC slab. The RC slab then acts as a diaphragm to distribute the loads to the concrete walls below. The RC walls on gridlines 1, 6, 8, 12, 14 and 18 then resist the majority of the lateral load through in-plane bending and shear. A number of bracing walls have been modified or removed since the building was originally built.

4.4.2 Longitudinal Loading

The lateral loads in the longitudinal direction are resisted through in plane action of timber and RC walls. Timber framed bracing walls transfer the lateral loading from the roof level to the ground floor RC slab. The RC slab then acts as a diaphragm to distribute the loads to the concrete walls below. The RC walls on gridlines B, D, I, J, K, M, N and O then resist the majority of the lateral load through in-plane bending and shear. A number of bracing walls have been modified or removed since the building was originally built.

4.5 Original Documentation

Copies of the following drawings were provided by the client and have been used in the seismic assessment of this building.



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- Grey Hospital Obstetric Block (Structural Drawings), prepared by Bruce-Smith Chapman & Amos, Consulting Civil & Structural Engineers, dated November 1977, sheets S1 to S70.
- Grey Hospital Obstetric Block (Architectural Drawings), prepared by Porter and Martin, dated August 1977, sheets 9 to 12, 18 to 27 and 32 to 34.
- Grey Base Hospital Redevelopment Acute Mental Health & Community Mental Health Services, Hopkinson Team Architecture Ltd, dated August 2000, sheets WD-A-415 to WD-A-437 and WD-A-499

The available drawings have been used to confirm the structural systems on-site, investigate potential Critical Structural Weaknesses (CSW's) and identify details which required particular attention. INFOR

5 **Building Inspection**

5.1 Visual Inspection

Visual inspections of the building were carried out by Jason Davidson of Opus on 31 July, 12 September and 13 September 2012. The purpose of these visual inspections was to verify information in the drawings and note changes or variations so that they could be considered in the seismic evaluation of the building.

A reinforcing bar scanner was also used during these visual inspections to verify position and spacing of reinforcing bars noted on the structural drawings.

Some intrusive investigation was also carried out during these inspections. The purpose of the intrusive investigation was to verify the construction details of the timber bracing walls so that an accurate bracing capacity value can be used during analysis. Intrusive investigation was also used to verify reinforcing steel in one of the RC piers and one of the RC columns, both at lower ground level.

5.2 **General Observations**

The building generally appears to be in a reasonably good condition with some areas of concern noted:

- There is cracking and possibly spalling of concrete on the vent sills in the lower ground floor external walls on gridline K between gridline 1 and 8. This type of deterioration has also been identified elsewhere in the hospital.
- There is extensive cracking in lower ground floor walls surrounding the storage area • between gridline 1 and 8 and gridline K and M. These walls have been plastered and it



West Coast District Health Board – Acute & Community Mental Health Services Building, Greymouth Detailed Engineering Evaluation

is unclear the reason why.

• The brick veneers at lower ground level are typically pulling away from the concrete walls. The first floor veneers were not inspected for this issue during this inspection.

6 Detailed Seismic Assessment

The detailed seismic assessment has been based on the NZSEE 2006 [2] guidelines for the "Assessment and Improvement of the Structural Performance of Buildings in Earthquakes" together with the "Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury, Part 2 Evaluation Procedure" [3] draft document prepared by the Engineering Advisory Group on 19 July 2011, and the SESOC guidelines "Practice Note – Design of Conventional Structural Systems Following Canterbury Earthquakes" [5] issued on 21 December 2011.

6.1 Critical Structural Weaknesses

The term Critical Structural Weakness (CSW) refers to a component or structural feature of a building that could contribute to increased levels of damage or cause premature collapse of a building. The following potential CSW's have been identified in this building.

a) Based on the intrusive testing of two timber bracing walls, it was identified that the walls are GIB lined but do not have bolted fixings to the concrete floor. They are nailed to the floor with Ramset or similar fasteners. We believe the walls are unlikely to meet the NZS3604:2011 requirements for fixing to the floor. As a result, it is possible that the walls may be overturned or slide along the floor during a seismic event, limiting their lateral load carrying capacity.

6.2 Quantitative Assessment Methodology

The probable seismic performance of the building has been assessed in accordance with the recommendations of the NZSEE publication "Assessment and Improvement of the Structural Performance of Buildings in Earthquakes" [2] dated June 2006 (Including Corrigendum No.1). The following sections in particular have been used in this assessment:

Section 7 "Detailed Assessment of Reinforced Concrete Structures"

Section 11 "Detailed Assessment Timber Structures".

The probable Earthquake loading for this building has been calculated from NZS 1170 -Structural design actions, Part 5 Earthquake Action [1]. The building has been classed as Importance Level 2 (IL2) in accordance with AS/NZS1170.0 as the client has advised that it is not critical for this building to remain operational post–earthquake.



Detailed Engineering Evaluation

The building has been assessed using a force based approach by applying the forces that may be expected to be applied to the building by the design earthquake. Calculations were made in respect of several wall elements of the building in order to assess their likely performance in an earthquake. This performance has been measured as a %NBS (New Building Standard), that is as a percentage of the capacity that would be required for the design of an equivalent new building on this site.

As the building can be considered to be irregular in plan, a 3D model of the building has been developed using the structural analysis software ETABS. A modal response spectrum analysis was undertaken to capture the effect of the irregular form on the building response to earthquake actions, including the effects of the higher dynamic mode shapes.

6.3 Limitations and Assumptions in Results

Our analysis and assessment is based on an assessment of the building in its original condition.

The results have been reported as a %NBS and the stated value is that obtained from our analysis and assessment. Despite the use of best national and international practice in this analysis and assessment, this value contains uncertainty due to the many assumptions and simplifications which are made during the assessment. These include:

- The normal variation in material properties which change from batch to batch.
- Approximations made in the assessment of the capacity of each element.

6.4 Seismic Coefficient Factors

The following seismic coefficient factors have been used in the evaluation of this building:

- Design life of building = 50 years, refer NZS1170.5 [1].
- Soil class C (shallow), refer NZS1170.5 [1] and Grey Base Hospital Geotechnical Assessment Report [8].
- Building Importance Level 3, refer AS/NZS1170.0.
- Seismic risk factor R_u = 1.3
- Seismic zone factor Z = 0.37, refer NZS1170.5
- Ductility μ = 1.5 (reinforced concrete) and 1.25 (timber framed bracing walls)
- Parts Acceleration in accordance with Section 8 of NZS1170.5 to calculate the seismic forces on the ground floor timber framed walls.


Detailed Engineering Evaluation

6.5 Material Properties

Assessments of material strengths have been based on limited drawings and site inspections. Characteristic material properties have been typically based on NZSEE guidance [2] and the Transit New Zealand Bridge Manual [7]. Probable material strengths have been used for the assessment of member capacities in accordance with NZSEE guidance [2].

The following probable material properties have been used in the assessment:

- f'_c = 25MPa (concrete nominal compressive strength)
- f_y = 275MPa (reinforcing steel nominal yield stress)

Based on the intrusive testing conducted on the timber bracing walls, it was found that the bracing walls are GIB lined, but do not have bolted fixings to the concrete floor. Instead they are nailed to the concrete floor slab. Hence the conservative valued strength of 3kN/m with a strength reduction factor of 0.7 provided in Table 11.1 of NZSEE guidance [2] was adopted. This is comparable to the bracing unit rating of GS1-N and GS2-N, both of which do not require additional end hold down fastenings and are rated to have 60 bracing unit per metre (3kN/m). [9]

We understand from information provided that a bracing schedule was not completed during the c.2000 refurbishment. Therefore it appears that the new internal walls were designed and constructed as internal partitions only and not as bracing walls. However, we have assumed that these c.2000 internal walls have a nominal bracing capacity as the drawings indicated that they are lined with 9.5mm GIB board and that the hold-down detail is likely to be equivalent or better than the original timber bracing wall.

The following soil characteristics have been provided by Hayden Bowen from Tonkin and Taylor for assessing the capacity of the shallow pad foundations:

• Minimum ultimate bearing strength of ground = 210kPa.

6.6 Quantitative Assessment

A summary of the structural performance of the building is shown in the following table. Note that the values given represent the worst performing elements in the building, as these effectively define the building's capacity. Other elements within the building may have significantly greater capacity when compared with the governing elements. This will be considered further when developing the strengthening options.



Detailed Engineering Evaluation

Structural Element/System	Failure mode or description of limiting criteria based on capacity of critical element.	Critical Structural Weakness and Collapse Hazard	% NBS based on calculated capacity
Concrete walls below ground floor – East West direction	In plane bending and shear of concrete walls.	No	100%
Concrete walls below ground floor – North South direction	In plane bending and shear of concrete walls.	No	100%
Timber framed bracing walls at ground floor – East West direction	In plane bending and shear of timber framed walls.	No	15%
Timber framed bracing walls at ground floor – North South direction	In plane bending and shear of timber framed walls.	No	19%

Table 6.1: Summary of Seismic Performance

6.7 Discussion of Results

The quantitative assessment of this building indicates that the building has the following seismic capacity:

- Seismic capacity in transverse direction (East West direction) = 12%NBS.
- Seismic capacity in longitudinal direction (North South direction) = 15%NBS.

The seismic capacity of the concrete framed and walled structure below ground floor has been assessed to be >100%NBS.

The predicted lateral deflection of the ground floor slab under the design seismic event is less than the 25mm gap provided due to the relatively stiff wall structure. This deflection is well within the 2.5% code drift limit. The small deflection and the fact that the stairs are constructed integrally with the adjacent RC walls means that the stairs are unlikely to be subject to additional loads (and subsequent damage or loss of function) due to being rigidly connected to both levels.

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The seismic capacity of the building is governed by the capacity of timber framed bracing walls on the ground floor level to transfer the lateral load from the roof to the ground floor diaphragm in both the East-West and North-South direction. The bracing capacities of the timber framed bracing walls are limited due to the uncertainty in the hold-down capacity and nailing pattern of the walls. We believe that the nailed fixing to the floor slab will not allow the full ductile bracing capacity of the timber framed walls to be achieved, rather that the wall may rock or slide over the slab once the nailed fixings become overstressed.



Detailed Engineering Evaluation

Based on the assessed %NBS, this building is classified as Earthquake Prone.

It is expected that the building will sustain significant wall damage above first floor level under a design level earthquake (1000 year return period). The rocking or sliding of the timber framed walls is still expected to be a ductile type of failure, therefore we do not believe the building poses a collapse risk.

As this building is Earthquake Prone, GDC policy [6] requires strengthening work to improve the building performance to a minimum of 67%NBS to be completed within 12 years.

7 Summary of Geotechnical Appraisal (Tonkin and Taylor [8])

7.1 General

The Geotechnical Appraisal of the Acute & Community Mental Health Services Building is based on structural drawings provided by the WCDHB and the Geotechnical Assessment Report prepared for the Canterbury District Health Board by Tonkin and Taylor [8]. The drawings indicate the RC walls are supported on a continuous strip footing and RC columns are supported on isolated pad footings which are linked together by RC groundbeams.

The strip footing is typically 1.0m wide and is founded 1.0m below the ground surface. The isolated pad footings vary in size and are linked together with a 450mm wide groundbeam.

7.2 Geotechnical Appraisal

Based on the Geotechnical Assessment Report the area should be classed as a shallow soil site, ground class C in terms of NZS1170.5. The assessment result was based on four machine drilled boreholes to a maximum depth of 18.45m below ground level with Standard Penetration Tests (SPTs) at 1.5m intervals. Mudstone bedrock was encountered in two of the boreholes at depths of 15m and 17m below ground level.

The soil profile at the site was found to be 0-3m medium dense sand and gravel overlaying 3-12.5m of soft silt. Beyond that is very dense gravel.

7.3 Summary and Recommendations

The town of Greymouth has a high risk of intense seismic shaking. Associated with this shaking risk are some secondary earthquake risks that are site specific such as liquefaction.

The Grey Base Hospital site is identified as having a low potential for liquefaction induced ground damage. This is due the high permeability and density of the gravel and the high fine grain particles of the soft silt layers. Hence both layers are considered to be non-liquefiable.



Detailed Engineering Evaluation

As a result, liquefaction and lateral spreading damage is not expected in an ULS earthquake at the site. Any differential settlement would be due to large cyclic loads causing permanent settlements of the foundations. These differential settlements are hard to quantify, but generally are reasonably minor and should not cause any issues from an ULS perspective.

8 Remedial Options

The Acute & Community Mental Health building is Earthquake Prone and therefore requires strengthening under the Building Act. According to the Earthquake Prone building policy adopted by the GDC, it is required to be strengthened to a minimum of 67%NBS or be demolished within 12 years [6].

Possible strengthening concepts to improve the seismic performance of the building could include the following:

- Develop a bracing plan, calculating the length, type and location of new bracing elements required on the first floor, and
- Remove existing first floor timber framed wall linings, install required hold-down restraints at the base of the wall and re-line walls with GIB bracing, or
- Install steel straps with hold downs over the top of existing timber walls to act as bracing bays. Note that given the obtrusive nature of this strengthening option, it is unlikely to be a suitable long term solution.

9 Conclusions

The seismic performance of the Acute & Community Mental Health Services building has been assessed as:

- Seismic capacity above ground floor in the transverse direction (east west) = 15%NBS.
- Seismic capacity above ground floor in the longitudinal direction (north south) = 19%NBS.
- Seismic capacity below ground floor in both directions = 100%NBS

The building is therefore classed as Earthquake Prone as it has a seismic capacity of less than 33%NBS.

It is expected that the building will sustain significant damage under a design level earthquake (500 year return period) and the building is classed as a "high risk" building. However we do not believe that it poses a collapse risk.



Detailed Engineering Evaluation

This building requires strengthening in accordance with the policy adopted by GDC [6], to a minimum of 67% NBS or be demolished within 12 years.

10 Recommendations

We recommend that a staged strengthening approach as detailed below is followed in order to understand and manage the economic impact of any proposed remedial actions. Specifically we recommend that:

a) The implications of the IL2 classification for this building be carefully considered prior to carrying out any future works on this building, noting that with an IL2 classification, this building is not expected to remain operational post-disaster.

An IL2 classification may also limit future use of the building.

- b) An outline scheme for structural strengthening with a view to achieving at least 67%NBS should be further developed followed by costing by a quantity surveyor.
- c) A quantity surveyor is engaged to determine the costs for strengthening the building.
- d) Detailed design of a scheme for the strengthening of the structure is carried out.

In addition to the seismic strengthening scheme, there are several issues that were identified during the inspection that warrant further investigation:

- There is cracking and possibly spalling of concrete on the vent sills in the lower ground floor external walls on gridline K between gridline 1 and 8. This type of deterioration has also been identified elsewhere in the hospital and we recommend that chloride intrusion testing be carried out. This will help to identify whether there are any major issues with concrete deterioration of the building.
- There is extensive cracking in lower ground floor walls surrounding the storage area between gridline 1 and 8 and gridline K and M. These walls have been plastered and the reason why is unclear. This may indicate some underlying issue which we recommend be investigated further.
- The brick veneers at lower ground level are typically pulling away from the concrete walls behind. This may be due to the corrosion of galvanised tie wires behind the brick veneers. It is recommended that some brickwork be removed to allow for inspection of the tie-back and the investigation of other possible causes for the separation. The ground floor brick veneers were not inspected and we recommend that any further investigation / inspection include these also.



Detailed Engineering Evaluation

11 Limitations

- a) This report is based on a visual inspection of the structure of the Acute & Community Mental Health Services building and a quantitative assessment of the building.
- b) Our professional services are performed using a degree of care and skill normally exercised, under similar circumstances, by reputable consultants practicing in this field at this time.
- c) This report is prepared for WCDHB to assist with assessing the seismic capacity of this building. It is not intended for any other party or purpose.

12 References

[1] NZS 1170.5: 2004, *Structural design actions, Part 5 Earthquake actions,* Standards New Zealand.

[2] NZSEE: 2006, Assessment and improvement of the structural performance of buildings in earthquakes, New Zealand Society for Earthquake Engineering.

[3] Engineering Advisory Group, *Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury, Part 2 Evaluation Procedure*, Draft Prepared by the Engineering Advisory Group, Revision 5, 19 July 2011.

[4] Engineering Advisory Group, *Guidance on Detailed Engineering Evaluation of Nonresidential buildings, Part 3 Technical Guidance*, Draft Prepared by the Engineering Advisory Group, 13 December 2011.

[5] SESOC, *Practice Note – Design of Conventional Structural Systems Following Canterbury Earthquakes*, Structural Engineering Society of New Zealand, 21 December 2011.

[6] Grey District Council, *Earthquake-Prone, Dangerous and Insanitary Buildings Policy,* Adopted 14 February 2011.

[7] Transit New Zealand: *Bridge Manual*, Second Edition 2003 (including amendments).

[8] Grey Base Hospital Geotechnical Assessment prepared by Tonkin & Taylor Ltd for Canterbury District Health Board, August 2012. T&T Ref: 53097

[9] GIB, GIB EzyBrace Systems 2011, July 2011

[10] AS/NZS 1170.0: 2002, *Structural design actions, Part 0 General Requirements,* Standards New Zealand.



PHOTOGRAPHS PHOTOGRAPHS



Detailed Engineering Evaluation

Acute & Hospita	& Community Mental Health Services Building – Grey Base al
No.	Photo
Gen	eral
1.	North elevation
2.	West elevation
3.	East elevation
4.	Roof level
5.	Extensive cracking in lower ground walls surrounding storage area
6.	Cracking of concrete on the vent sills in the lower ground floor external walls
7.	Brick veneers pulling away from concrete walls
8.	Intrusive testing of first floor timber walls

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Detailed Engineering Evaluation





Photo 2: West elevation

Doc Ref: 6-WCAN1.02 / 185GG



Date: 28 September 2012

MAC Photo 3: East elevation

Photo 4: Roof level

Doc Ref: 6-WCAN1.02 / 185GG



Date: 28 September 2012

Detailed Engineering Evaluation



Photo 6: Cracking of concrete on the vent sills in the lower ground floor external walls



Detailed Engineering Evaluation



MALMARMATIONACK Photo 7: Brick veneers pulling away from concrete walls



Photo 8: Intrusive testing of first floor timber walls



Appendix B DRAWINGS



Acute & Community Mental Health Service Building – Grey Base Hospital No. Drawings General 1. S2 - Grey Hospital Obstetric Block, Foundation Plan S3 – Grey Hospital Obstetric Block, Basement Plan 2. 3. S4 – Grey Hospital Obstetric Block, Lower Ground Floor Plan S5 – Grey Hospital Obstetric Block, Ground Floor Layout 4. S7 - Grey Hospital Obstetric Block, Perimeter Wall on Line 6 5. S9 – Grey Hospital Obstetric Block, Interior Columns From Basement Level 6. 7. S25 – Grey Hospital Obstetric Block, Perimeter Walls on Line B S50 - Grey Hospital Obstetric Block, Ground Floor Beams Lines C & D 8. 9 – Grey Hospital Obstetric Block, Sections F-F – K-K 9. 10. 10 – Grey Hospital Obstetric Block, Sections L-L – Y-Y 11. 12 – Grey Hospital Obstetric Block, Brickwork Details, Concrete Finishes 12 20A -Grey Hospital Obstetric Block, Ground Floor Partitions & Strapping Plan & Details 13. 21 – Grey Hospital Obstetric Block, Timber Roof Beams Plans 14. 24 – Grey Hospital Obstetric Block, Ground Floor Ceiling Framing Plan 15. WD-A-402 – Grey Base Hospital Redevelopment, Construction Plan





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The COPYRIGHT of these drawings and the ideas contained therein remain the property of the author unless otherwise agreed in writing.

The Contractor shall verify all dimensions onsite before work is commenced. All work is to comply with NZS3604:1999 and the New Zeatand Building Code

Zealand Building Code Unless stated otherwise, all dimensions are in millimetres

Do Not Scale - use Dimensions only

This d	This drawing is to be read in conjunction with ail others					
Revis	ions.	n an				
Rev.	Date.	Details.				
2	30 May 2000 23 Jul 2000	Issued for Construction Door 59 altered, New wall in Mc60 Note 40 & 41 adde Duct noted in Mc11 Window shifted over on dec Notes 29 & 33 molfield notes removed UCU area revised doors 95,95 added, windows 53, 54 addee, Rooms Mc17 Mc37 Mc6 addee MC16 Techocated Dimensions added, dexik Mc12 relocated, existing ramp detend, Mc62 Mc63 shower detend, Mc62 Mc61				
3	24 NOV 2000	Wash Hand Basins to Rooms Mc68,69,70,71,73,74,75,76, 79,80,81 removed internal ducts for downpipes added				



Appendix C

JGY AFLEASED UNDER THE OFFICIAL QUANTITATIVE ASSESSMENT METHODOLOGY AND ASSUMPTIONS



Reinforced Concrete Walls and Frames

C1. **Analysis Parameters**

The following parameters are used for the seismic analysis:

- AAC Cl. 3.1.3, NZS1170.5 Site soil category C (shallow soil) Cl. 2.2.14_B, B1/VM1
- Seismic hazard factor Z = 0.37
- Table 3.5, NZS1170.5 Return period factor $R_u = 1.0$ (Importance Level 3 structure, 50 year design life)
- Cl. 2.6.1.2, NZS3101:2006 Ductility factor $\mu = 1-1.5$
- Material properties (based on Transit New Zealand Bridge Manual Section 6)

Concrete nominal compressive strength, <i>f</i> ['] _c (MPa)	25
Mild reinforcing nominal yield strength, <i>f_y</i> (MPa)	275

Table C1: Analysis Material Properties

Effective section properties

Table C6.6 - Effective section properties, Ie Type of member Ultimate limit state Serviceability limit state $f_{v} = 300 \text{ MPa}$ $f_{v} = 500 \text{ MPa}$ μ = 1.25 $\mu = 3$ $\mu = 6$ 1 Beams (a) Rectangular[¶] 0.7 Ig 0.40 Ig 0.32 Ig 0.40 Ig I_g (use with E₄₀) § (use with E40) § (use with E_{40})[§] T and L beams 0.6 Ig 0.35 Ig 0.27 Ig I_{g} 0.35 Ig

	(use with E_{40}) ³	(use with E_{40}) ³			(use with E_{40}) ³
2 Columns					
(a) $N^*/A_g f'_c > 0.5$	0.80 $I_{\rm g}$ (1.0 $I_{\rm g}$) [‡]	0.80 Ig (1.0 Ig) [‡]	I _g	1.0 Ig	As for the
(b) $N^*/A_g f'_c = 0.2$	$0.55 I_{g} (0.66 I_{g})^{\ddagger}$	$0.50 I_g (0.66 I_g)^{\ddagger}$	Ig	0.8 Ig	ultimate limit
(c) $N^*/A_g f'_c = 0.0$	$0.40 I_g (0.45 I_g)^{\ddagger}$	0.30 $I_{\rm g}$ (0.35 $I_{\rm g}$) [‡]	Ig	0.7 <i>I</i> g	state values in brackets
3 Walls ¹					
(a) $N^*/A_g f'_c = 0.2$	0.48 Ig	0.42 <i>I</i> g	Ig .	0.7 Ig	As for the
(b) $N^*/A_g f_c = 0.1$	0.40 Ig	0.33 Ig	Ig	0.6 Ig	ultimate limit
(c) $N^*/A_q f_c = 0.0$	0.32 Ig	0.25 Ig	Ig .	0.5 Ig	state values
4 Diagonally reinforced coupling beams	$0.6I_g$ for flexure Shear area, A_{shear} ,	as in text	Ig 1.5 A _{shear} for ULS	0.75 Ig 1.25 A _{shear} for ULS	As for ultimate limit state
NOTES – (§) With these values the	ne <i>E</i> value should be th	e elastic modulus for co	oncrete with a str	rength of 40 MPa re	gardless of the actual

tual

The values in brackets apply to columns which have a high level of protection against plastic hinge formation in the ultimate (\pm) limit state.

For additional flexibility, within joint zones and for conventionally reinforced coupling beams refer to the text. (1)

TableC2: Effective section properties from NZS3101:2006

(b)

Detailed Engineering Evaluation

- Earthquake load combination $G + E_u + \Psi_E Q$
- Floor live loading Q = 3.0 kPa
- Earthquake combination factor $\Psi_E = 0.3$
- Building seismic weight $W_t = G + \Psi EQ$ Wt = 27,650 kN

C2. Assessment Methodology

Static & Modal Response Spectrum Analysis

Cl. 4.2.2, AS/NZS1170.0

Table 3.1 Part G, AS/NZS1170.1

Table 4.1, AS/NZS1170.0

Cl. 4.2, NZS1170.5

The seismic assessment was undertaken by completing static and Modal Response Spectrum (MRS) analyses for the building in accordance with NZS 1170.5:2004.

A 3D model was set up using the structural analysis program ETABS, and effective section properties for structural members were taken from Table C2 above. The first floor timber walls were not modelled. The ground floor slab was modelled as rigid diaphragms and the roof was also modelled as a rigid diaphragm for load distribution.



Figure A4.1: ETABS model of Acute & Community Mental Health Building

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The fundamental building periods output from ETABS are:

Building	Period -E/W direction (s)	Period –N/S direction (s)
Community and Mental Health Building	0.05	0.06

Table C3: Fundamental periods

A total of 35 modes are used in the MRS analysis resulting in 97.6% and 98.8% effective participating mass in the E/W and N/S directions, respectively.

An equivalent static analysis was also carried out as a consistency check of the MRS analysis output. As the structure is irregular, the base shear from the MRS analysis was scaled up the equivalent static method base shear, as required by NZS1170.5, Clause 5.2.2.2. The base shears resulting from the equivalent static method are:

Building	Base shear -E/W direction (kN)		Base shear –N/S direction (kN)	
	Equivalent Static	MRS	Equivalent Static	MRS
Community and Mental Health	19950	12150	19950	13550

Table C4: Base shear from analysis

The forces from the MRS analysis were scaled up by 1.64 and 1.47 in the E/W and N/S directions, respectively. The design actions were applied separately in each perpendicular direction as required by NZS1170.5, Clause 5.3.1.1.

Timber walls

C3. Analysis Parameters

The following parameters are used for the seismic analysis:

٠	Site soil category	Cl. 3.1.3, NZS1170.5
	C (shallow soil)	
٠	Seismic hazard factor	Cl. 2.2.14 _B , B1/VM1
	Z = 0.37	
	Return period factor	Table 3.5, NZS1170.5
\checkmark	$R_u = 1.0$ (Importance Level 3	structure, 50 year design life)
•	Part risk factor	Table 8.1 NZS1170.5
	$R_{p} = 1.0$	
٠	Ductility of the part	Table 8.2 NZS1170.5
	μ = 1.25	
٠	Period of the part	Estimated
	$T_{p} = 0.4$	
•	Bracing capacity	Table 11.1 NZSEE
	Gypsum wall board, unblocked edge	es $3kN/m$ each side ($\Phi = 0.7$)



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- Roof dead load (framing + cladding)
 G = 0.75 kPa
- Roof live loading Q = 0.25 kPa
- Earthquake combination factor $\Psi_E = 0.3$

Estimated

Table 3.2 R2, AS/NZS1170.1

Table 4.1, AS/NZS1170.0

C4. Assessment Methodology

The diaphragm system in the roof is the GIB board ceiling. It is considered as a flexible diaphragm system and hence the seismic forces will be distributed roughly based on tributary area to its adjacent load resisting element.

To calculate the seismic forces acting on the timber walls, the total roof area that can be distributed to the exterior concrete walls was subtracted out the total roof area. It was then multiplied by the seismic mass and the parts acceleration factor in accordance with section 8 of NZS1170.5 assuming a ductility factor of 1.25.

The total seismic force was then divided by 2.1kN/m (0.7 x 3kN/m) to calculate the total length of wall required as the GIB walls are fairly evenly distributed. The length was wall required was compared to the length of wall provided to come up with a %NBS.





BUILDING WARRANT OF FITNESS

T	IE BU	ILDING					
Street address of Building: 71-111 Waterwalk Road Greymouth					Legal Description of land where building is located: Rateable Portion of res 1014 2001 2007 2089 Pt Sec 494 499 1707 Greymouth		
Bi Gi Tr	iilding ey Ba aining	Name: Ise Hospita])	l (Main building, kitchen, G	P	Locat Main	ion of Building within site/block number: Entrance – off high street	
Le	vel/Ur	nit Number:	N/A		Curre	nt, Lawfully established use:	
Ye 20	ar firs 07	t constructe	d		Intend	ded life of the building (if 50 years of less): inite	
Hi	ghest	fire hazard o	category for building use: 2		Com	liance Schedule No.: 184	
TH	IE OW	/NER				2	
Na	ime of est Co	Owner: ast District	Health Board		Conta Ph	9(2)(a) 9(2)(a)	
AC	ENT:			_		.0'	
Na Re	me of lations	Agent: S P ship to Own	GS NZ Ltd O Box 8032 Christchurch er: Duly Authorised Agent	8440	Addre Phone Email	ess: 151B Waterloo Road Christchurch 8042	
SY	STEN	IS - as pe	r Building Act 2004		0		
~	1	Automatic	Systems for Suppression of	f fire	14/1 14/2	Emergency power systems for, or signs relating to, a system or feature specified in any systems 1 to 13	
~	2	Automatic systems f	or manual emergency warn	ing 🗸	15/2	Final Exits and Other Exit Doors	
< <	3/1 3/3	Electroma windows	gnetic or automatic doors or	*	15/3	Fire Separations Protecting a Means of Escape	
V	4	Emergend	y Lighting systems	1	15/4	Signs for Communicating information intended to Facilitate Evacuation	
1	8/1	Passenge	r Lifts	2.41 1.3			
NA	RRAI	NT	V.				
The	e maxi	imum numb	er of occupants that can safe	ly use this	building	is: GP Training 15 Hospitak< 500	
The full	e inspe / com	ection, main plied with du	tenance, and reporting proce uring the 12 months prior to t	edures of the date sta	ne comp ated belo	pliance schedule for the above building have been	
The	Com	pliance Sch	edule is kept at: 71-111 Wa	terwalk Ro	ad Grey	mouth	
AT	ГАСН	MENTS:	a) Certificates relating to in b) Recommendations for a	spections, mendment	mainter ts to the	nance, and reporting (Form 12A compliance schedule, if any.	
Sig 9(2)(1	natur	e Owner / o	r Authorised Agent: N	lame:	9(2)(a)	17.6.19	

This document is issued in accordance with SGS's General Conditions for Inspection and Testing Services and should be read subject to them (copy available on request of at http://www.sgs.com/terms_and_conditions.htm).


Inspection Date: 12.06.19



dormakaba

dormakaba New Zealand Ltd 61-69 Patiki Road Avondale,1026 Auckland New Zealand Ph: 0800 788 688 www.dormakaba.com.nz

FORM 12A

Certificate of Compliance with Inspections, Maintenance and Reporting Procedures Form 12A Section 108 (3) (c), Building Act 2004

The Building

Legal Land Description: 1707 GREYMOUTH Building Name: Building Address: CS Number: Owner Details: Contact Person: RATEABLE PORTION OF RES 1014 2001 2007 2089 PT SEC 494 499

Grey Base Hospital 71-111 Waterwalk Road Greymouth 7805 184 West Coast District Health Board, PO Box 387, Greymouth 7840

Compliance:

The inspection, maintenance and reporting procedures of the Compliance Schedule have been fully complied with during the 12 months prior to the date stated below in relation to the following specified systems/s:

SS3/1 - Automatic Doors

Comments/Remedial Action:

Name of Company: dormakaba NZ Limited

Signature:

Date:

June 12, 2019

dormakaba New Zealand Ltd

9(2)(a)

www.dormakaba.com.nz

Ph: 0800 436 762



CERTIFICATE OF COMPLIANCE WITH INSPECTIONS, MAINTENANCE AND REPORTING PROCEDURES

FORM 12A Section 108 (3)(c), Building Act 2004

TH	E BUI	LDING				
Street address of Building: 71-111 Waterwalk Road Greymouth				Legal Description of land where building is located: Rateable Portion of Res 1014 2001 2007&2089 Pt Sec 494 499 1707 Greymouth		
Building Name: Grey Base Hospital (Main Building Kitchen & GP Training)				Location of Building within site/block number: Main Entrance – Off high street		
Level/Unit Number:				Annual BWOF Expiry Date: 1 July 2020		
				Compliance Schedule No.: 184		
TH	EOW	NER	-			
Name of Owner: West Coast District Health Board				Contact Person:		
Mailing Address: Po Box 387 Greymouth 7804				Street Address/Registered Office:		
COMPLIANCE				71-111 Waterwalk Road Greymouth		
The	inspe ing the	ction, maintenance, and reporting procedure 12 months prior to the date stated below i	es of n rel	f the com ation to t	pliance schedule have been fully complied with he following specified system/s:	
SPI	CIFIE	D SYSTEMS AS PER BUILDING ACT 200	4			
~	3/3	Interface fire or smoke doors or windows	**	14/1 14/2	Emergency power systems for, or signs relating to, a system or feature specified in any systems 1 to 13	
~	4	Emergency Lighting systems	J	15/2	Final Exits and Other Exit Doors	
~	7	Automatic backflow preventers connected to a potable water supply	1	15/3	Fire Separations Protecting a Means of Escape	
~	8/1	Passenger Lift	1	15/4	Signs for Communicating information intended to Facilitate Evacuation	
Co	nmer	nts:				
Name of Licensed Building Practitioner (Please Print):					9(2)(a)	
Nan Con	ne of L npany	BP/IQP SGS NZ Ltd				
Signature of Licensed Building Practitioner:					Date: 6/6/2019	

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